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A new design of stepped antenna loaded metamaterial for RFID applications

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ABSTRACT

Radio frequency identification is being overloaded with data information, making wideband band antennas very appealing. In this paper, we present a new design of dual band antenna for RFID reader applications operating at 2.45Gz and 5.8GHz with an average gain of 1.16dB at the lower frequency band and 3.2dB at the higher frequency band. The antenna is designed on an FR-4 substrate having a relative dielectric constant of 4.4 and loss tangent of 0.025. The proposed antenna is simulated, designed and, optimized using CST Microwave Studio and has a small size of 32 mm x 26 mm x 1.6 mm. The antenna consists of a steeped rectangular patch antenna using a partial ground plane loaded a modified split ring resonator. The metamaterial structure was designed and optimized to operate at 2.45GHz and its effective parameters was verified using the Nicolson-Ross Weir method. The performance of the proposed antenna is confirmed by another 3D electromagnetic solver HFSS.

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1. INTRODUCTION

In recent years, the telecommunications field has known an extremely rapid development. This development driven by strong demand from industry and consumers has led to the emergence of radio communications circuits. Among these technologies we find the radio frequency identification (RFID) which knows today its full development. It affects several sectors and has a wide range of applications, such as distribution, logistics, security, traceability, identification and so on [1]-[5].

The RFID technology is basically a wireless communication that allows the identification of objects of all types, including humans and animals, by radio waves data capture. The objects are identified thanks to a specific label, called tag, embedded the object to be identified [6]-[8]. Depending on the application, RFID systems operates at different frequencies from the HF band around 13kHz to the microwave band around 2.45GHz and 5.8GHz [9]-[12].

Generally, a typical RFID system consists of two main components, a transponder and a reader. The transponder is a device comprising an electronic microchip for storing data and an antenna for communicating with the reader, each tag containing a unique identification information of the tagged object. The reader is a device that communicates with the transponder through an antenna, it can read and write information on the RFID chip. An RFID system can be represented by the block diagram of Figure 1 [13]-[16]. Antennas are a very important factor in communication between reader and tag in RFID systems. They require antennas with good performance and a miniature size; however, it is very difficult to design antennas with good performance and small size at the same time. For this reason, different techniques are

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proposed in many researches to reduce the size of antennas without degrading their performance, such as fractal geometry, the use of slots, folding techniques, and so on. [17]-[21].

In this work, we proposed to use metamaterial structures that are subwavelength structures having some electromagnetic characteristics which do not exist in conventional materials. The rest of this paper is organized as; in the second section, we present de proposed metamaterial structure, in third section, we presented the antenna design and in the last section, the results and discussion will be reported.

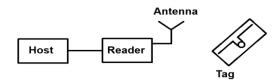


Figure 1. Block diagram of an RFID system

2. PROPOSED METAMATRIAL STRUCTURE

Metamaterials are artificial materials with electromagnetic properties that cannot be found in nature. The theoretical concept of metamaterials was introduced for the first time by Veselago in 1968 [22]. But the experimental concept for producing negative permittivity materials from metallic wires was proposed by Pendry *et al.* in 1996 [23]. Three years later, Pendry and his colleagues proposed to take advantage of the inductive response of the collective electron movement in non-magnetic conductive elements in the form of a split ring resonator (SRR) to achieve a negative permeability [24].

Based on Pendry's work, several publications have studied new structures and analyzed the left-hand behavior of these structures, such as circular, rectangular, triangular, and so on. In this paper, we present a new miniature metamaterial structures based on modified split ring resonators. The proposed structure is illustrated in Figure 2 (a) and its optimized parameters are illustrated in Table 1. In order to verify the metamaterial effect of this structure, it has been introduced into a waveguide box as shown in Figure 2 (b).

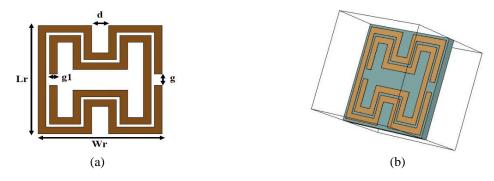


Figure 2. These figures are; (a) geometry of the proposed metamaterial resonator, (b) proposed metamaterial resonator in a TEM waveguide box

Table 1. Dimensions of the proposed metamaterial resonator parameters

Parameter	Dimension (mm)
Wr	19.5
Lr	19.5
g	2
g1	1.2
d	2.6

The simulation results in terms of reflection and transmission coefficients are presented in Figure 3 (a). It is clearly remarkable that this structure works around 2.45GHz which is the targeted frequency at designing the antenna. The Nicolson Ross Weir method was used to extract the actual parameters. This method makes it possible to extract the permittivity and permeability based on the S-parameters results using the [25].

$$S_{11} = \frac{i}{2} \left(\frac{1}{z} - z \right) \sin(nkd) \tag{1}$$

$$S_{21} = \frac{1}{\cos(nkd) - \frac{i}{2}(z + \frac{1}{z})\sin(nkd)}$$
 (2)

$$z = \sqrt{\frac{(1+S_{11})^2 - S_{21}^2}{(1-S_{11})^2 - S_{21}^2}} \tag{3}$$

$$\varepsilon_{eff} = \frac{n}{z}$$
 and $\mu_{eff} = nz$ (4)

Where n is the refractive index, z is the wave impedance, k is the wave number, d is the thickness of the metamaterial unit cell, ϵ is the electric permittivity, and μ is the magnetic permeability. The computed results in terms of permittivity are presented in Figure 3 (b). We can notice that the proposed structure presents a negative primitivity between 2Ghz and 2.5GHz.

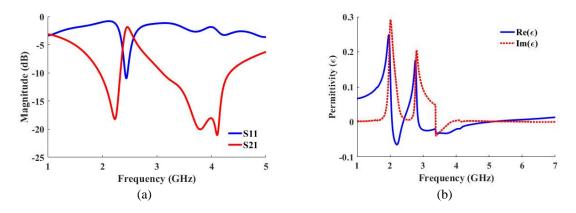


Figure 3. These figures are; (a) S-parameters of the proposed metamaterial resonator, (b) permittivity of the proposed metamaterial resonator

3. ANTENNA DESIGN

The proposed antenna is composed of a rectangular patch with two steps to improve the bandwidth around operating frequencies. The bottom part of the antenna is composed of a partial ground plane loaded by a metamaterial structure in order to reduce the overall size of the antenna. Figure 4 illustrates the proposed antenna geometry. The antenna is designed on an FR-4 substrate having a thickness H=1.6 mm, a relative dielectric constant ϵr =4.4, and tangent losses $\tan(\delta)$ =0.025. The overall size of the proposed antenna is 26mm × 32mm and the metallization thickness is 35 µm. The operating frequencies of the antenna are 2.45GHz and 5.8GHz. The optimized antenna parameters are summarized in Table 2.

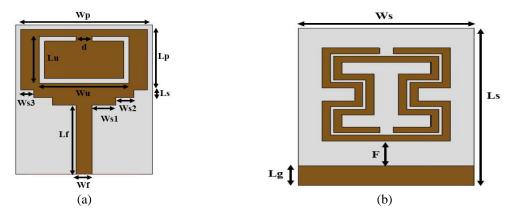


Figure 4. Geometry of the proposed antenna, (a) top view, (b) bottom view

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Table 2.	Dimensions	of the	proposed	antenna
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Parameter	Dimension (mm)
Ws	26
Ls	32
Wp	24
Lp	13
Wu	17
Lu	10
Ws1	4.5
Ws2	3.5
Ws3	2.5
Ls	1.6
D	3
Lf	18
Wf	3
Lg	4

4. RUSULTS AND DISCUSSION

The computed results in terms of reflection coefficient are illustrated in Figure 5. As can be seen, this antenna operates around the two bands 2.45GHz and 5.8GHz which are regularized for RFID technology. The antenna has a wide bandwidth ranging from 2.4GHz to 2.66 GHz for the first band and ranging from 5.74GHz to 6.14GHz for the second band with a good impedance matching about -25dB around 2.45Ghz and -46dB around 5.8GHz.

The radiating patterns of the antenna in the E and H planes are shown in Figures 6 and 7. It is noted that two radiation sides are favored, radiation in front of the antenna due to the patch and radiation in the back of the antenna is due to the metamaterial structure. The surface current distribution is plotted in Figure 8. It is remarkable that the maximum of the surface currents is around the open ring and the steps at the bottom of the patch at 5.8GHz and it is maximal around the metamaterial cell at 2.45GHz. The gain over the frequency of this antenna is plotted in Figure 9. It has a good gain of 1.3 dB at the first resonance frequency and 3.8 dB at the second resonance frequency.

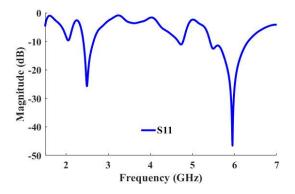


Figure 5. Reflection coefficient of the proposed antenna

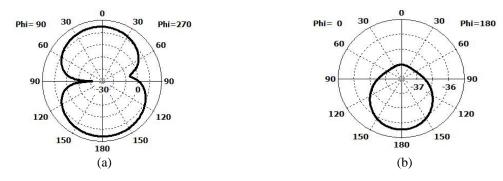
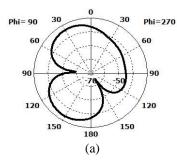


Figure 6. Radiation pattern of the proposed antenna at 2.45 GHz, (a) H-plane, (b) E-plane



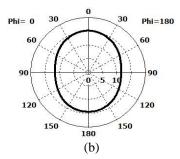


Figure 7. Radiation pattern of the proposed antenna at 5.8 GHz, (a) H-plane, (b) E-plane

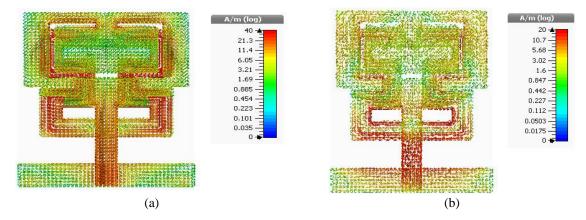


Figure 8. Current distribution of the proposed antenna at, (a) 2.45GHz, (b) 5.8GHz

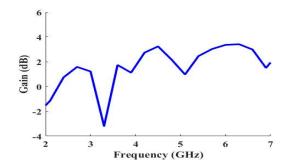


Figure 9. Gain over frequency of the proposed antenna

5. CONCLUSION

In this paper, a dual-band antenna for RFID applications using a partial mass plan loaded by a new metamaterial structure was presented. The metamaterials cell has been studied in order to extract its effect parameters to verify its metamaterials effect. The proposed antenna was designed on an FR4 substrate having a relative permittivity of 4.4 and tangential losses of 0.025. It has a miniature size of 32mm x 26mm x 1.6mm and good performance. The presented antenna has a good gain of 1.3dB at the first frequency band and 3.8 dB at the second frequency band. Wide bandwidths about 230MHz at 2.45Ghz and about 400MHz at 5.8 GHz were achieved using steps at the bottom of the patch. This antenna is a good solution for RFID handheld applications.

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